





#### PART I of II

Introduction

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Mission Design

Spacecraft System

Command and Data Handling

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### Introduction

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### Mission

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#### **STEREO Objectives**

- Understand the origin and consequences of coronal mass ejections (CMEs)
- Determine the processes that control CME evolution in the heliosphere
- Discover the mechanism and sites of polar energetic particle acceleration
- Determine the 3-D structure and dynamics of coronal and interplanetary plasmas and magnetic fields
- Probe the solar dynamo through its effects on the corona and heliosphere





#### Implementation Responsibilities

#### • JHU/APL

- Provide spacecraft bus, instrument integration,
   mission design, mission operations, and navigation
- Manage DSN interfaces
- Manage spacecraft to instrument interfaces

#### • GSFC

- Provide and operate instruments
- Provide and operate Science Operations Center
- Launch vehicle procurement





#### **Space Weather Monitoring**

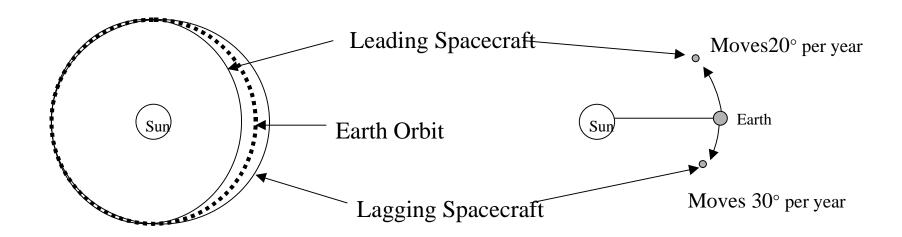
- Whenever not in contact with 34-m DSN assets, transmit a low-rate (≈500 bps) science stream that is available to space weather enthusiasts
- All on-board science data processing to be provided by the instruments
- No knowledge of the data content is required by the spacecraft
- A description of the intended ground assets and required downlink rate will be provided by GSFC
- Space weather downlink is not to drive telecommunication design





#### **Mission Design Overview**

- One spacecraft orbit less than 1 AU; other orbit greater than 1 AU
- As viewed in a fixed Sun–Earth frame; each spacecraft slowly moves away from Earth







#### **Spacecraft Overview**

- Both spacecraft are identical
- 3-axis controlled
- Propulsion for momentum management, no orbitmaintenance requirement
- Single-string with two year primary mission
- Parts/components designed for two year mission duration
- Consumables for five year mission duration
- Design should not preclude extended mission





#### **Operations Overview**

- Decoupled spacecraft/ instrument operations
- Daily contacts (seven per week) using 34-m DSN antennas, with the beam-waveguide (BWG) antennas as prime
- Single Mission Operations Center (MOC) to control both spacecraft at JHU/APL
- All operations planning, spacecraft status, and navigation information to be posted on the internet





### **Spacecraft Operations Concept**

- Spacecraft has one operational mode: point at Sun and antennas at Earth
- Thruster firings, used for momentum management, occur at ≈4–10 day intervals
- Most spacecraft operations are autonomous
  - High-gain antenna pointing control
  - Momentum management
  - Power management
  - Thermal management
- On-board recorder management is ground controlled





#### **Instrument Operations Concept**

- Instrument operation including health monitoring is a GSFC responsibility, spacecraft operations is a JHU/APL responsibility
- Science team (GSFC) should not need to know any of the details of spacecraft *operation* to plan instrument activity
  - Small time windows budgeted for HGA movement and propulsive events
  - Instrument activity independent of downlink schedule
  - Stored-command memory budgeted for instrument operations
- Spacecraft has resources (power, data bandwidth) to support all instrument activity simultaneously with the only limitation being data volume





### Mission Design

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#### **Science Orbit Definition**

- Orbit configuration is defined by the desired time history of the spacecraft angular separation
  - Absolute spacecraft separation viewed from the Sun
  - Relative spacecraft separation from the Earth-Sun line
- Desired time history of separation defined by dwell angle and duration from Science Definition Team Report (pg. 30)
  - Leading Spacecraft
    - Drifts ahead of the Earth in its orbit
    - $-20^{\circ}$  from Earth T = 200 to 400 days
    - $-45^{\circ}$  from Earth T = 600 to 800 days
  - Lagging Spacecraft
    - Follows behind the Earth in its orbit
    - $-30^{\circ}$  from Earth T = 200 to 400 days
    - $-60^{\circ}$  from Earth T = 600 to 800 days





#### **Launch Vehicle Requirements**

- Launch vehicle provides direct insertion into desired heliocentric orbit
  - Launch energy (C3) requirement limited by launch vehicle and insertion stage motor selection
  - Departure asymptote declination limited by launch vehicle and insertion stage motor selection
  - \* No maneuvers by spacecraft to achieve or maintain orbit
- Launch opportunity window (TBD)
- Daily launch window (TBD)





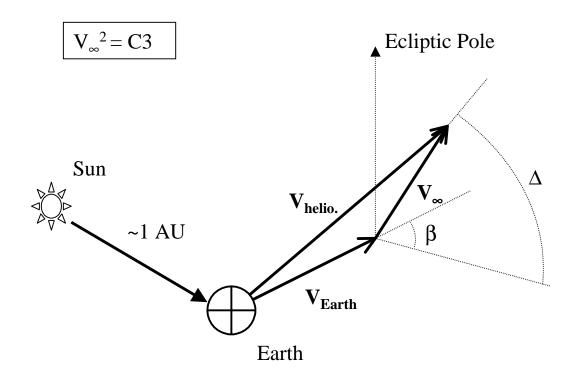
#### **Preliminary Mission Design**

- Athena-II Expendable Launch Vehicle
  - 93° Launch azimuth
  - Eastern range (CCAS/KSC) launch site
  - STAR-37 upper stage
  - Preliminary ascent timeline provided by Lockheed-Martin
  - $C3 = 1.0 \text{ km}^2/\text{sec}^2$
- Launch Dates
  - Leading October 1, 2002
    - Smallest drift rate ⇒ minimize impact of launch delays for second spacecraft
    - Closer to equinox ⇒ minimize Sun-Probe-Earth angle for RF design
  - Lagging December 1, 2002





#### **Launch Parameter Definition**







### Preliminary Mission Design (cont'd)

- Leading Spacecraft
  - Design parameters
    - $C3 = 1.0 \text{ km}^2/\text{sec}^2$ ,  $\beta = -41^\circ$ ,  $\Delta = 49^\circ$
  - $C3 > C3_{min} \approx 0.3 \text{ km}^2/\text{sec}^2$ 
    - Reduce sensitivity to launch vehicle dispersions
    - Tailor Sun-Probe-Earth angle characteristics for RF design
  - $-\beta$  selected maximize dwell time at desired separation angle
  - $\Delta$  selected to tailor Sun-Probe-Earth angle characteristics for RF design
  - Departure asymptote declination,  $\delta = -28^{\circ}$ 
    - $\delta$  with respect to equator
    - Maximum achievable declination (absolute value) for Athena-II with 93° launch azimuth (maximum launch mass)
  - Mean drift rate relative to Earth-Sun line =  $20^{\circ}$  per year





### Preliminary Mission Design (cont'd)

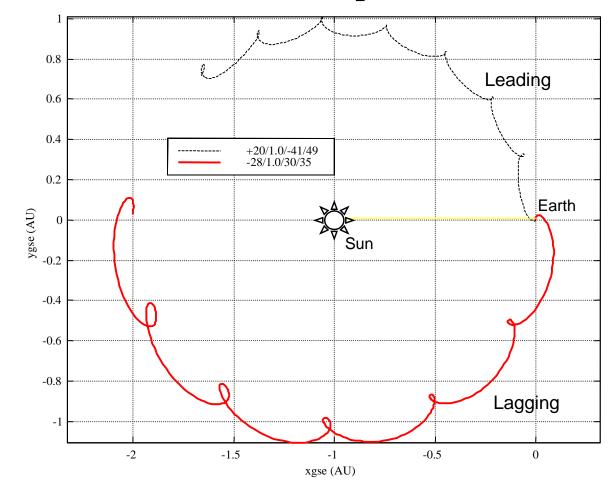
- Lagging Spacecraft
  - Design parameters
    - $C3 = 1.0 \text{ km}^2/\text{sec}^2$ ,  $\beta = 30^\circ$ ,  $\Delta = 35^\circ$
  - $C3 > C3_{\min} \approx 0.6 \text{ km}^2/\text{sec}^2$ 
    - Reduce sensitivity to launch vehicle dispersions
  - $-\beta, \Delta$ 
    - Launch phase definitions identical to leading
    - Impacts to dwell time/separation behavior (TBD)
  - Departure asymptote declination,  $\delta = -28^{\circ}$
  - Mean drift rate relative to Earth-Sun line =  $28^{\circ}$  per year





#### **STEREO Orbit**

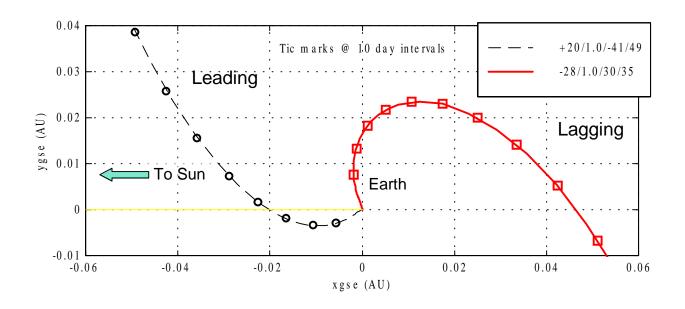
#### (Geocentric Solar Ecliptic Coordinates)







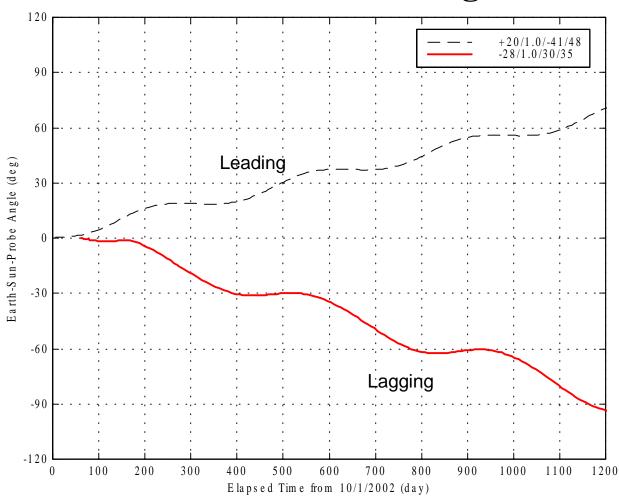
#### STEREO Orbit Detail (Geocentric Solar Ecliptic Coordinates)







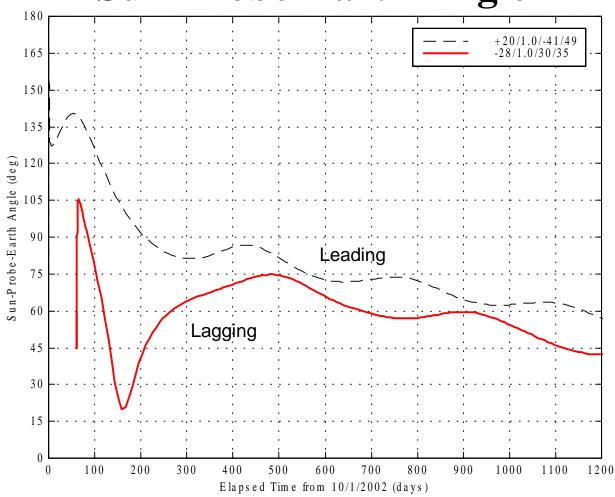
#### **Earth-Sun-Probe Angle**







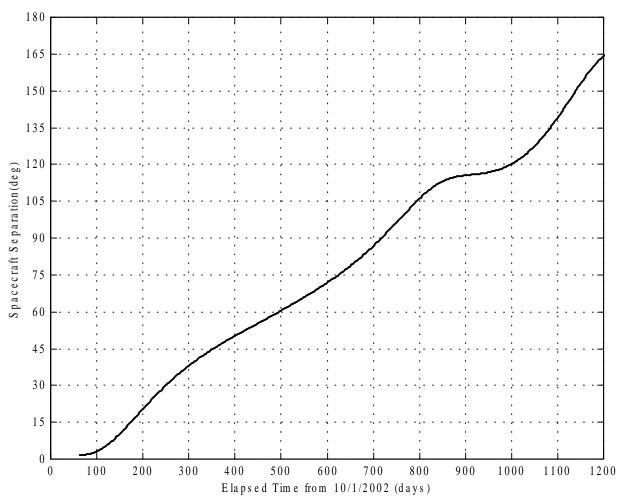
#### **Sun-Probe-Earth Angle**







### **Spacecraft Separation (Alpha angle)**







### Spacecraft System

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#### **Outline**

- Orbits
- Top level and autonomy requirements
- Block diagram
- Sparing philosophy
- Phase A studies
- Technology insertion candidates





#### **Required Orbits**

- Leading spacecraft: Lead the Earth at a rate of ~20°/year with a dwell near 20° between 200 and 400 days and one at 45° between 600 and 800 days.
- Lagging spacecraft: Lag the Earth at a rate of ~30°/year with a dwell near 30° between 200 and 400 days and one at 60° between 600 and 800 days.





### **Spacecraft Requirements**

- Conceptually, the instrument suite on each STEREO spacecraft consists of a:
  - Solar Coronal Imaging Package, Radio Burst Tracker,
     Heliospheric Imager, Solar Wind Plasma Analyzer, Magnetometer,
     Energetic Particle Detector.
  - In operational mode, instruments operate at 100% duty cycle.
  - The exact instrument compliment will not be known until well into Phase A.
- Solar images are taken simultaneously (±1 sec) from the two spacecraft.
- Support the instrument suite with power, commands, telemetry and unobstructed views for instruments and their radiators.

99-0316-4 Spacecraft System ASD **4** 





### **Spacecraft Requirements (Con't)**

- The SCIP instrument will provide an error signal to the S/C Attitude Control System. Meet LV interface requirements.
- Spacecraft warns instruments prior to shut off and momentum dump. Instrument survival heaters remain powered.
- Support autonomous LV to operational mode transitioning.
- Maximum time difference of 0.5 seconds between spacecraft.
- Maximum mass 350 kg including 20% margin going into Phase A.
- Maintain full operational mode for Sun/z-axis angle of ±5° or less.





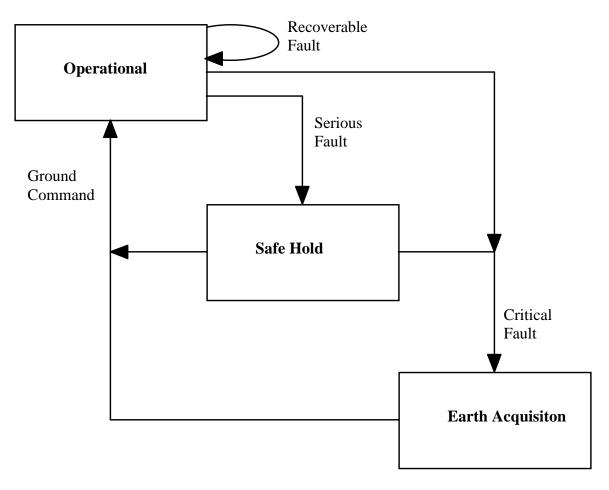
#### **Spacecraft Autonomy Requirements**

- The spacecraft will have an autonomous safe-hold mode where the Z-axis is controlled to within 1° of the Sun and the MGA is held within 1° of Earth.
- The spacecraft will have an autonomous Earth-acquisition mode where the Z-axis axis is controlled to within  $1^{\circ}$  of the Sun and rotation about the Sun line is controlled to  $1^{\circ}$ /minute  $\pm 0.5$  min/revolution.
- Provide an autonomous Sun-keep-in capability where the Sun angle is programmable.
- Return to <5° of Sun pointing in <12 minutes from any attitude after any rates have been nulled to zero.
- Capable of autonomously re-positioning the HGA for optimal gain within pre-specified windows. May be overridden or altered from the ground.
- Capable of autonomously momentum dumping within pre-specified windows. May be overridden or altered from the ground.
- Autonomous power management
- Passive thermal control.





#### **Initial Spacecraft State Design**



#### **Operational**

- Enabled time-tag commands
- All instruments on
- Sun point with all antennas toward Earth
- Telecom over HGA

#### Safe Hold

(Roll-axis knowledge of assumed)

- Suspend time-tag commands
- Reset spacecraft state (instruments off)
- Sun point with antennas at Earth
- Telecom emergency rates over MGA

#### **Earth Acquisition**

(Roll-axis k nowledge not assumed)

- Suspend time-tag commands
- Reset spacecraft state (instruments off)
- Sun point and rotate 1 deg per minute
- Telecom emergency rates over MGA
- Recovery initiated with a stop-rotate command

99-0316-4 Spacecraft System ASD **7** 





#### Launch Vehicle

• The baselined launch vehicle for the STEREO mission is the Athena II.

Launch is separated by two months.

- Each spacecraft will be launched on a separate ELV.
- The shuttle will be studied as an alternative LV. Two spacecraft will be manifested on the same shuttle.
- JHU/APL will make a launch vehicle recommendation at the end of the Pre-Phase A study.





#### **Mission Lifetime**

• Designed for a two year mission with expendables designed to last for five years.

Mission time starts when both spacecraft are on orbit

• Do nothing to preclude a longer mission beyond two years.

Data rate will degrade past the 200 kb/sec at two years requirement

• Two years is the baseline mission duration.





#### Reliability/Redundancy

- Reliability: Standard JHU/APL reliability practices
- Redundancy: In order to minimize cost, the STEREO spacecraft will be of a single string hardware design based on the TIMED architecture and hardware.

Some inherent redundancy exists





#### **Spacecraft Differences**

- The two STEREO spacecraft will be form, fit, function and interface identical.
  - Eases build and integration
  - Can take advantage of lessons learned
  - One spacecraft can replace the other in schedule with minimal changes





#### **Radiation**

• Spacecraft hardware will be capable of operating for the mission duration in the environment outlined under the reference memo. This includes:

Component total dose hardness level of 10 Krad.

• All spacecraft electronics will be latch-up immune and SEU tolerant.

Reference: GSFC (Janet Barth) radiation environment analysis and Memo SOR-98048.





#### **Cleanliness**

- Handling and I&T Environment Class 100,000 during bus integration.
- Instrument selection may dictate the use of more stringent cleanliness requirements
- A Contamination Control Plan will be written after instrument selection and requirements have been defined.





#### **Communications**

- Science data volume requirement is 5 Gbit/day.
- Nominally, complete volume will be transmitted to the Earth within 24 hours

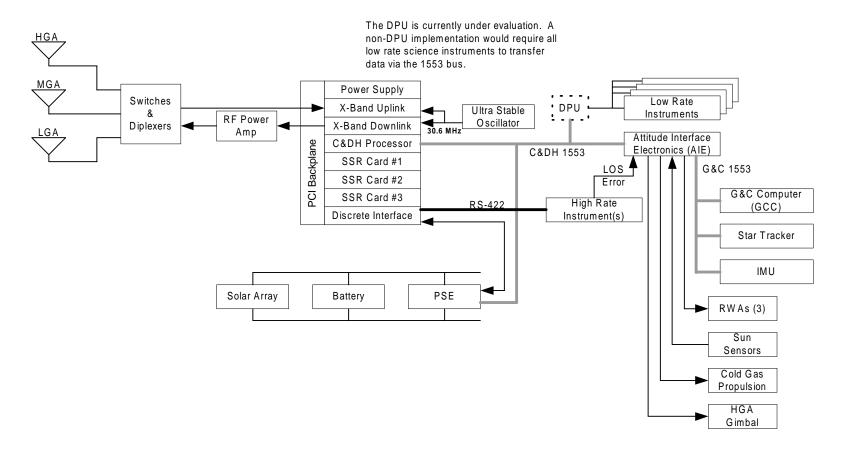
Data rates will vary with Earth probe distance.

- Maximum DSN pass time is 8-hours (at end of mission).
- Each STEREO spacecraft will support a low rate "broadcast mode" of 500 b/s which will be transmitted at all times, when not transmitting high rate data.





### **STEREO Block Diagram**







### Flight Spares Philosophy

- Sparing will occur only at the piece part level. There will be no one for one box level or procured hardware spares (except for battery).
- A spare flight board will be fabricated/purchased for all in house boards (except for the SSR). These boards will be left unpopulated. One set of components will be purchased for every two used.
- The goal is to minimize cost without undue schedule risk.
- Additional sparing will be considered on a case by case basis.





### **Current Requirements Deficiencies**

- Transmission gap between day 76 and 125 on the leading spacecraft.
- Minimum data rate at the end of two year mission 0.97 AU (Data rate is 82 kb/s). Day 661 drops below 200 kb/s (34m HEF).
- Jitter requirement—Additional analysis during Phase A required.





#### **Phase A Studies**

- G&C/Safing architecture trade
   Removal of AIU processor, RTX-2010 compiler is no longer supported.
- MiniMOCS
- Non rotisserie Safe Mode
   Using low gain antenna in safe mode in conjunction with 70 m DSN.
- Continue Jitter Analysis
- Communications gap





### **Technology Insertion Candidates**

- Momentum dumping via trimmable flaps
- Non-coherent navigation (baselined)
- LiIon battery
- Advanced recorder management
   File system





### **Command and Data Handling**

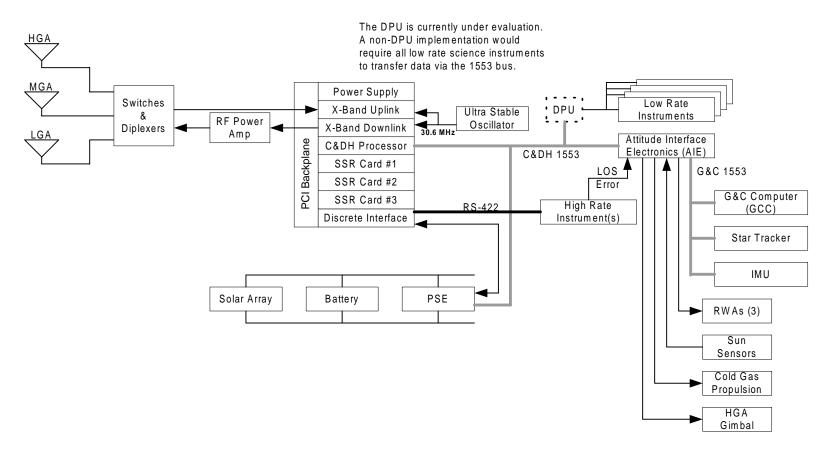
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#### **Spacecraft Block Diagram**







#### **C&DH** System Requirements

- Implementation requirement
  - Re-use TIMED architecture
- Functional requirements
  - Uplink command and stored command management
    - CCSDS compatible uplink
    - Provide for two data rates: 100 bits/sec and 7 bits/sec
  - Telemetry data processing
    - CCSDS compatible downlink
    - Provide for maximum data rate of 800 Kbits/sec (allows for transmission of 8 Gbits/3 hr DSN downlink time)





#### **C&DH** System Requirements (con't)

- Functional requirements
  - Mass storage of science and engineering data
    - 5 Gbit science volume + housekeeping + overhead and margin
    - Simultaneous and random read/write capability
    - Error management and graceful degradation
    - Interleave real-time data with recorder playback data, but optimized for science (e.g., 97% science data, 3% real-time products)
  - Support science data collection
    - Provide real-time downlink mode for instruments (one at a time)
    - Provide variable telemetry bandwidth allocation for instrument data, selectable by the science team
    - Provide "Broadcast Mode" data collection and transmission at 500 bits/sec when not transmitting high rate data
    - Support instrument combined maximum data generation rate (~410 Kbits/sec) for storage and real-time downlink

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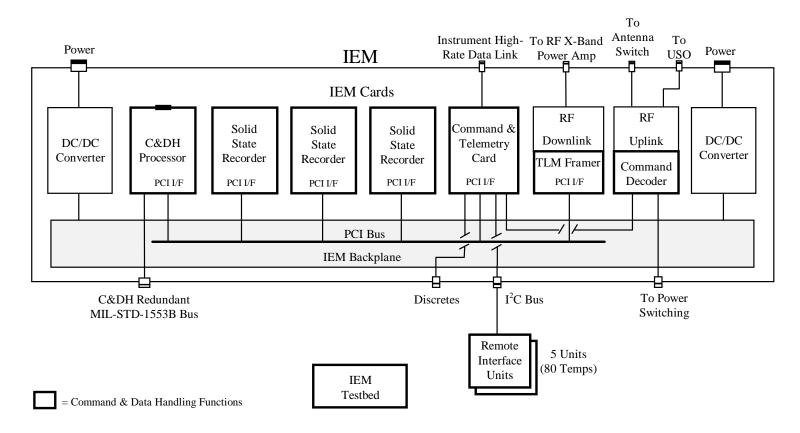
#### **C&DH** System Requirements (con't)

- Functional requirements (con't.)
  - Support engineering data collection
    - S/C temperatures, voltages currents and telltales
    - Non-coherent navigation data
    - Instrument status information
  - UT maintenance and distribution
    - 0.1 second accuracy
  - Autonomous fault protection
  - Manage subsystem intercommunication
    - C&DH MIL-STD-1553B bus controller





# Integrated Electronics Module (IEM) Configuration Baseline







#### **TIMED:** Processor and SSR Requirements and Capabilities

TIMED	REQUIREMENTS	CAPABILITIES
	_	
C&DH	32-Bit architecture	Mongoose V CPU clocked at 12 MHz
Processor	2MBytes SRAM	9.6 RISC MIPS throughput
	4MBytes EEPROM	
	MIL-STD-1553B redundant bus	
	PCI local bus	
Solid-State	1.9 Gbit Capacity	2.5Gbits Capacity
Recorder	4Mb/s Pk Read Rate	8Mb/s Pk Read Rate, 8Mb/s Pk Write Rate
	30Kb/s Pk Write Rate	Simultaneous R/W, 8Mb/s combined rate
	Random read/write capability	Random access at code block level
	Map around bad memory blocks	Settable, auto-incrementing R/W pointers
	Error management	Error management:
	Simultaneous read/write	Reed Solomon encoding with correction
		of up to 5 bytes with errors per block
		(245 bytes/block).
		Probability of >5 bytes in error per block is:
		$<10^{-21}$ , 24-hour scrub rate
		$<10^{-25}$ , 4-hour scrub rate
		memory error rate: <10 <sup>-12</sup> err/bit/sec





#### STEREO: Processor and SSR Requirements and Capabilities

STEREO	REQUIREMENTS	CAPABILITIES
C&DH	Same as TIMED	Same as TIMED
Processor		
a 11 1 a	5 Gbit + housekeeping + OH +	7.5Gbits capacity
Solid-State	Margin	8Mb/s Pk read rate, 8Mb/s Pk write rate
Recorder	750Kb/s Pk read rate	Simultaneous R/W, 8Mb/s combined rate
	450Kb/s Pk write rate	Random access at code block level
	Random read/write capability	Settable, auto-incrementing R/W pointers
	Map around bad memory	Error management:
	Error management: Max error rate	Reed Solomon encoding with correction of
	<10 <sup>-9</sup> bit errors/3-days	up to 5 bytes with errors per block (245
		bytes/block).
		Probability of >5 Bytes in error per block is:
		<10 <sup>-TBD</sup> w/scrub rate of every TBD-hrs
		memory error rate: <10 <sup>-TBD</sup> err/bit/sec





#### **Other IEM Internal Subsystem Functional Requirements**

Command &	Route uplink commands from the command decoder to the C&DH processor and	
Telemetry Card	C&DH processor relay commands to the command decoder	
	Collect S/C temperature data and IEM temp and voltage telemetry data	
	Provide interface for high rate instrument science data (RS-422)	
Downlink	Builds CCSDS compatible realtime, recorder, and null telemetry frames from data	
Framer	collected from the C&DH processor and the SSR and produces a serial data	
	stream to the RF modulator.	
	Timing chain and counter to provide 1 Hz time marking and MET, respectively	
	(clocked by S/C ultra-stable oscillator)	
Uplink	Receive CCSDS compatible commands from the Uplink Receiver command	
Command	detector (or from the GSE).	
Decoder	Route all commands to the C&DH processor, via the C&T subsystem.	
	Route all relay commands, either uplinked or generated by the C&DH processor,	
	to the power switching subsystem.	
	Perform autonomous load reduction upon receipt of a low bus voltage indication	
	from the power subsystem (execute a stored set of relay commands).	





#### **Candidate Studies**

- Solid-State Recorder–Make versus Buy
  - "Buy" considerations:

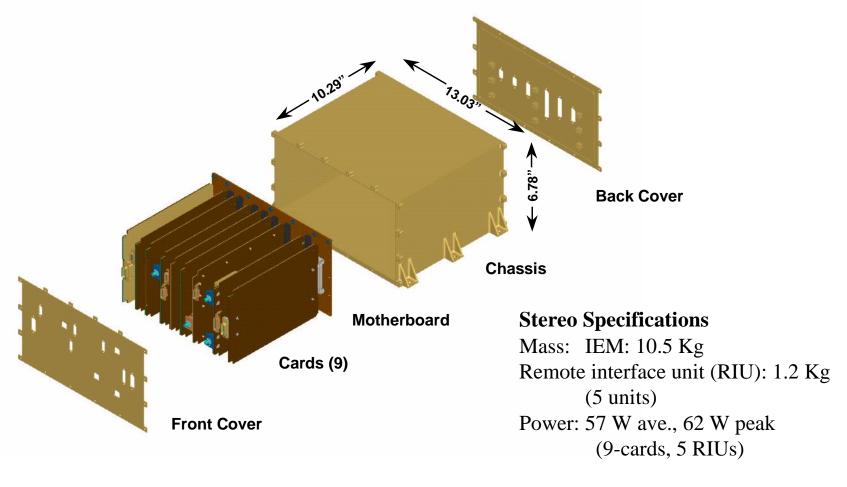
Acquire a unit that can be either interfaced to or inserted into the IEM.

- "Make" considerations:
  - Modified baseline—Upgrade the SSR using denser memory technology and/or packaging reducing it to a single card but with a 10 Gbit capacity.
- Temperature Remote I/O (TRIO) Chip-Technology Insertion
  - Compatible with existing IEM I<sup>2</sup>C bus system
  - Part packaging and qualification needs to be completed. Same part sought by JPL for use in X2000 program.





#### **TIMED IEM Chassis**







### **Guidance and Control**

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### **G&C** Requirements–Design Drivers

• Spacecraft pointing– $(3 \sigma)$ 

Roll Pitch/Yaw

- Knowledge:  $\pm 20$  arcsec  $\pm 0.1$  arcsec

- Control:  $\pm 0.1^{\circ}$   $\pm 20$  arcsec

- Jitter: 30 arcsec RMS 1.5 arcsec (0.1 to TBD Hz)

(with SCIP error signal, which is  $\pm 0.1$  arcsec)

- Jitter is challenge
- Need high control bandwidth =>
  - High wheel torque
  - Fast sampling rate
  - Minimize disturbances
  - Modern control techniques





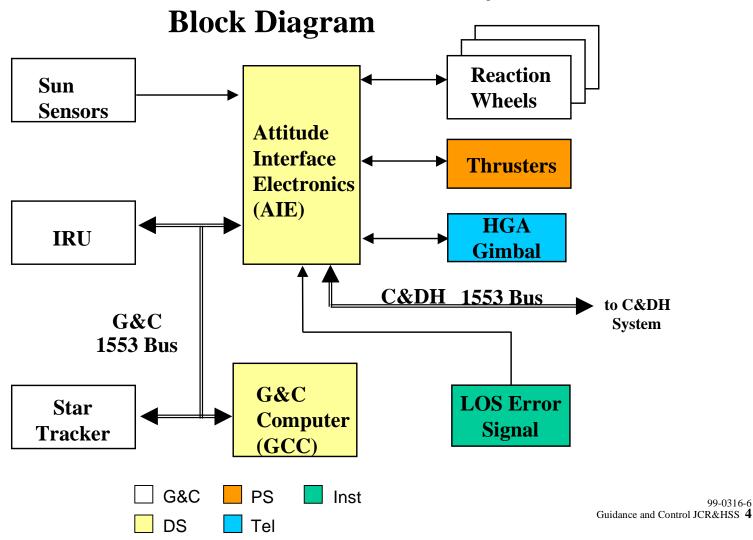
### **G&C** Requirements–Other

- Point LOS within 5 arcmin of Sun for SCIP acquisition
  - Requires good coalignment
- Nominal HGA pointing to 0.1°; maintain HGA pointing during thrusting; complete autonomous thruster firings within 300 seconds
  - Sets gimbal step frequency
  - Need small impulse bit and small  $\Delta t$
  - In-flight HGA alignment cal TBD
  - On-board ephemeris for HGA pointing vectors
- Momentum storage capacity > 4 days in operational mode
  - Sizes wheel momentum
- Return from any attitude in < 12 minutes
  - Thruster attitude control TBD
  - May size wheel torque
- Solar pressure momentum bias within Sun-angle limit





### **STEREO Guidance & Control System**







### **Baseline G&C Equipment**

Item	Heritage	Performance
IMU	NEAR	HRG, 0.01°/hr½
Star tracker	TIMED	3 arcsec, 7.5 Mv stars
Reaction Wheels	NEAR	Torque: 0.025 Nm
		Momentum: 4 Nms
Sun Sensors	NEAR	0.5° quantization
		0.25° accuracy
AIE	TIMED	
G&C Computer	TIMED	





#### **Inertial Reference Unit (IRU)**

- Supplier: Delco Electronics
- Gyros:
  - Delco 130Y Hemispherical Resonator Gyros (HRG)
  - Rate bias stability < 0.001°/hr, over 16 hr</li>
  - $ARW < 0.01^{\circ}/hr^{1/2}$
- Redundancy:
  - NEAR: redundant CPU, power; four gyros
  - Cassini: single-string
- Projected  $P_s$  (system function) = 0.9996 for mission life
  - (four gyro IRU)





### Reaction Wheel Assembly (RWA)

- Supplier: Ithaco, Inc. (Type A)
- Characteristics:
  - Brushless DC motor
  - Bipolar tachometer
  - Separate electronics, stacked to save weight and space
- Performance:

- Angular Momentum: 4 Nms (@ 5100 RPM)

- Torque: 0.025 Nm (higher torque possible)

- Unbalance:

static < 1.5 gm cm

dynamic  $< 40 \text{ gm cm}^2$ 

- Torque noise PSD:  $1 \times 10^{-11} \text{ (Nm)}^2/\text{Hz}, 0.1 \text{ to } 1 \text{ Hz}$ 

Continuous operating life: > 4 years





#### **Sun Sensors**

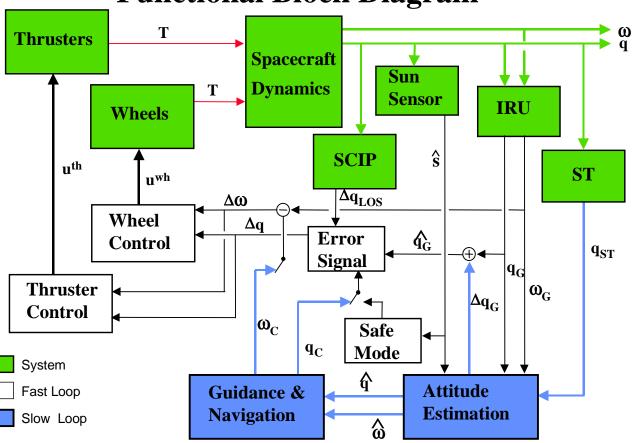
- Supplier: Adcole
- Digital Solar Attitude Detector (DSAD) system
  - Five detector heads, each measures 2-axis Sun vector in ±64° FOV
- Accuracy:
  - 0.5° quantization
  - 0.25° bit transition-angle accuracy
- Flight proven, many times





#### **Guidance & Control**

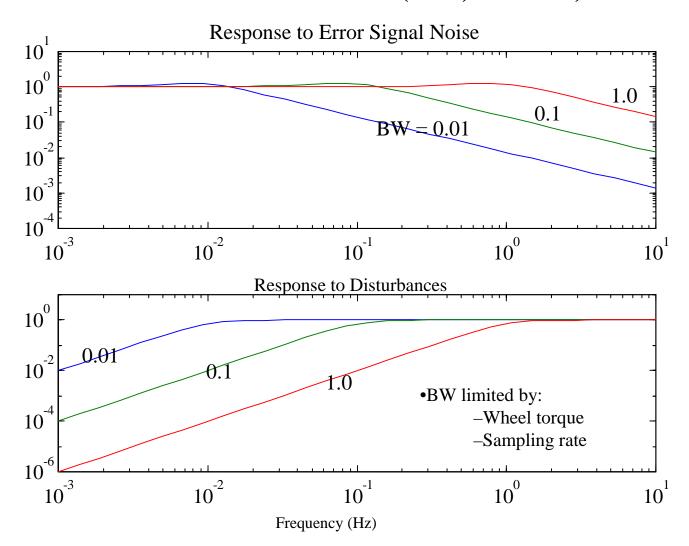
**Functional Block Diagram** 







#### Control Bandwidth (BW) Effects)



99-0316-6 ntrol JCR&HSS **11** 





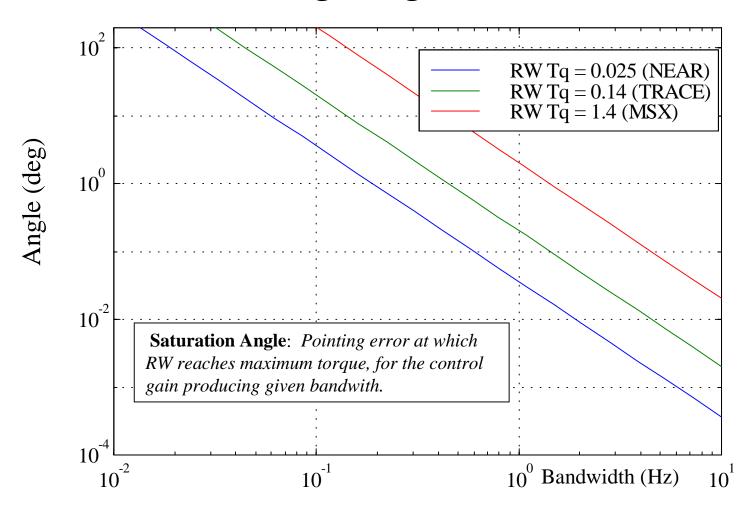
#### **Star Tracker**

- Supplier: Lockheed Martin
- Accuracy:
  - 3 arcsec P/Y; 32 arcsec R (1 $\sigma$ )
  - 7.5 My stars
  - 8.8° square FOV
- Quaternion output
  - Autonomous star ID within ~2 sec
  - 5 Hz update, 1553 interface
- Flown on DS1, P59; to fly on TIMED, EO1, MAP, IMAGE, ...





#### RW Saturation Angle (deg) vs. Control Bandwidth







### **Redundancy Considerations**

- Four Wheels
  - Full capability if any one fails
  - Enable wheel speed control to avoid troublesome frequencies
- Four Gyros
  - Full capability if any one fails
  - Lower noise if all four used
- Fine Sun Sensor
  - In addition to, or in place of, coarse DSADs
  - Enable mission pointing without LOS error signal
- ST gives some backup to LOS error signal





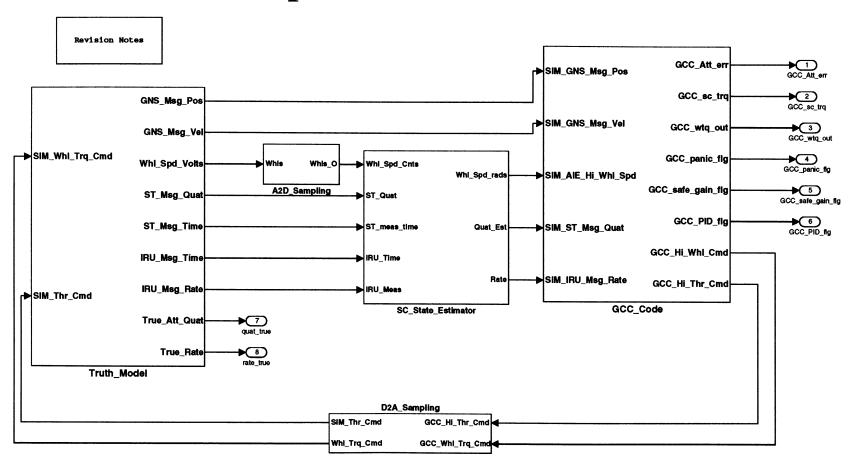
#### **Momentum Bias Mode**

- Possible for safe mode, or if y or z wheel fails—
  - x wheel runs at large fraction of its max speed
  - Other wheel(s) used to damp nutation
  - Precession by thruster firings
- Degraded pointing accuracy
  - Stability dominated by nutation
  - Accuracy limited by momentum precession
- Fuel for angular momentum precession:
  - About 150 mgm/day for 1°/day precession (H=4 Nms, Isp=65 s)
- If x wheel fails
  - y and z RW control still possible
  - Two-sided thruster limit cycle for x





#### **Top Level STEREO**

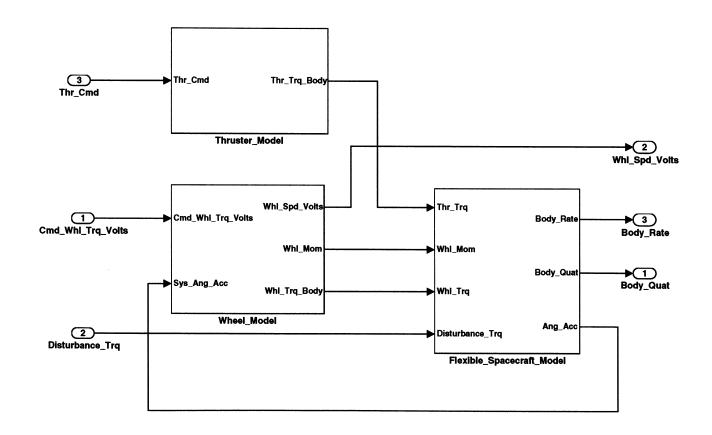






### **Preliminary STEREO Dynamics**

**Dynamics** 







### Flexible Spacecraft Dynamics

$$I\ddot{\theta} + M_{I}\ddot{\xi} = N - \dot{h} - \dot{\theta} \times (I\dot{\theta} + h + M_{I}\dot{\xi})$$
  
$$\ddot{\xi} + D\dot{\xi} + \Lambda\xi + M_{I}^{T}\ddot{\theta} = 0$$

where  $\xi$  -- modal coordinates of flexible structures;

 $M_I$  -- interaction matrix between flexible structures and rigid spacecraft body

 $M_I \dot{\xi}$  -- total momentum from flexible structures;

 $M_I \xi$  -- total acceleration from flexible structures;

 $D = 2k \cdot diag\{\omega_{f1},...,\omega_{fN}\}$  -- natural damping matrix of flexible structure;

 $\Lambda = diag\{\omega_{f_1}^2,...,\omega_{f_N}^2\}$  -- stiffness matrix of flexible structure.

#### **Assumptions:**

- Uniformly distributed beam like structure
- Normalized modal model, with lowest frequency  $f_0 = \frac{1}{2\pi} \sqrt{\frac{3EI}{(M+0.243\rho l)l^3}} Hz$ , and

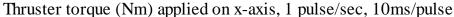
 $f_i = i \cdot f_0, i = 1,2,...N$ , based on preliminary structure parameters.

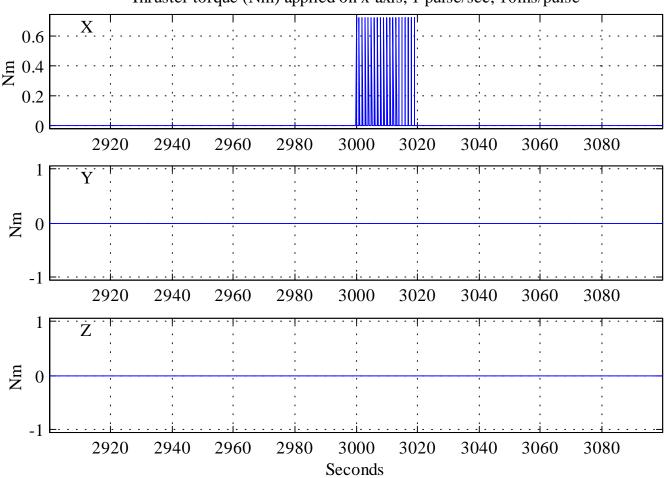
- Simplified interaction matrix, based on preliminary geometry of flexible structures
- Uncoupled flexible structure models
- No external force on flexible structures





#### Thruster Torque, Flexible Simulation

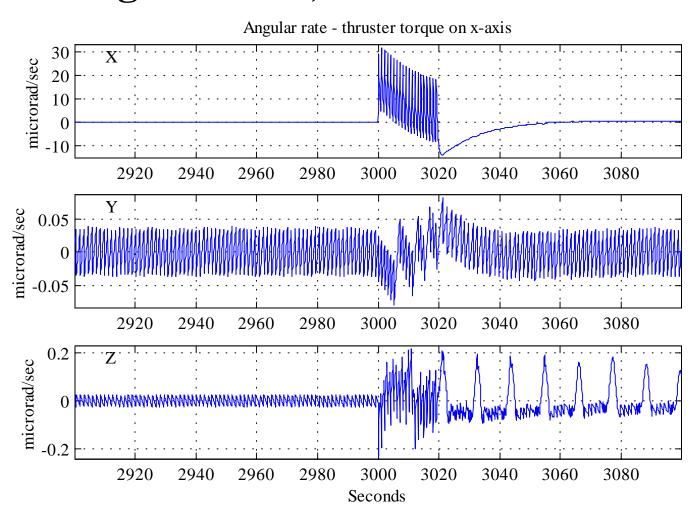








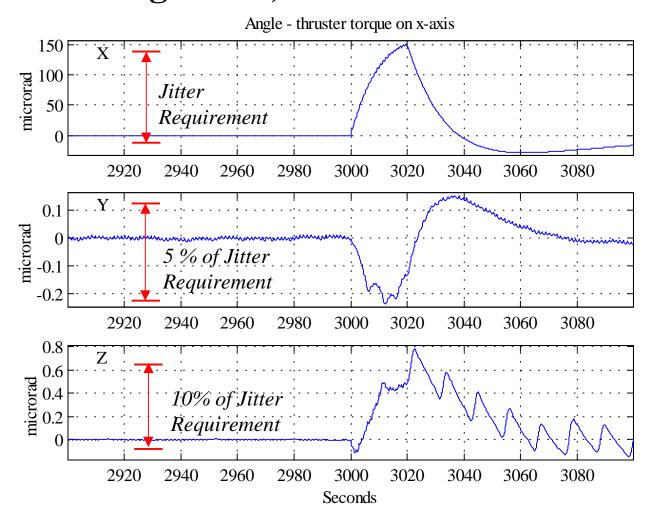
### **Angular Rate, Flexible Simulation**







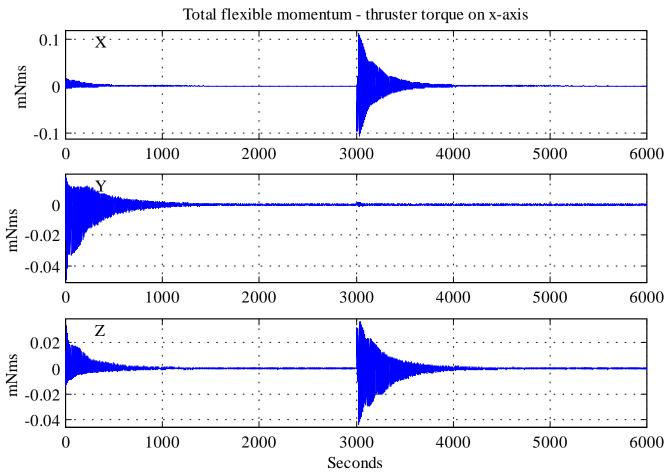
#### Pointing Error, Flexible Simulation







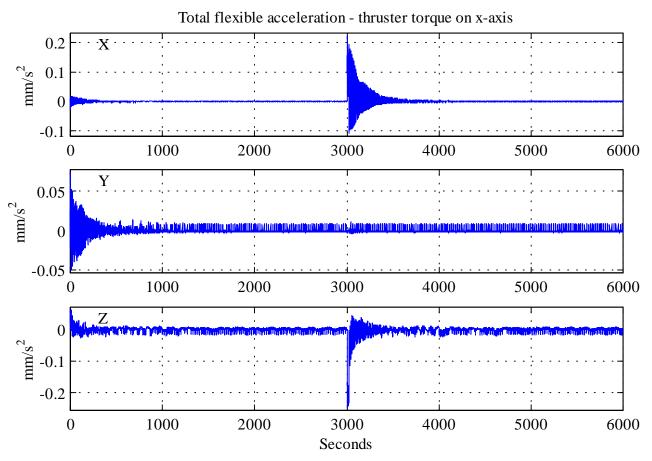
#### **Angular Momentum in Flexible Modes**







### Linear Acceleration, Flexible Modes







### Software

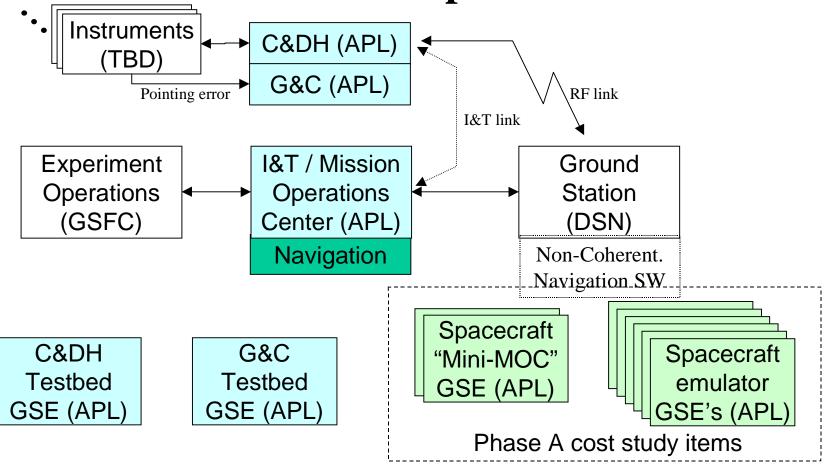
### Benjamin W. Ballard

The Johns Hopkins University Applied Physics Laboratory 11100 Johns Hopkins Road Laurel, MD 20723-6099





#### **Software Components**







### **C&DH S/W Requirements**

- Support CCSDS-compatible uplink/downlink
- Perform power management
- Perform spacecraft health and status monitoring
- Maintain and distribute time to 0.1 sec accuracy
- Allow for software upgrade capability
- Distribute commands to subsystems
- Support 7.5 Gbit recorder w/simultaneous record, playback
  - Dump entire recorder in 8-hours at 200 kbits/sec., or...
  - Dump recorder at max. downlink rate of 800 kbits/sec...
  - While continuing to record new data from science instruments at their maximum rates





### **C&DH S/W Requirements (con't)**

- Support science instruments
  - Provide "transparent" forwarding for instrument commands, telemetry
  - Provide limited space for instrument stored commands (~200 kbytes)
  - Label science and attitude history packets so they can be identified and routed to GSFC without inspection
  - Collect max rates (~450 kbps total) from all instruments simultaneously
  - Support "real-time" commanding and science downlink during ground contacts
- Support 500 bits/sec. "broadcast" telemetry mode
- No C&DH data compression is required





### **C&DH Requirements vs. TIMED**

Feature	TIMED	STEREO	Software Impact		
H/W redundant?	Yes	No	Requires new S/W loading approach		
GPS?	Yes	No	Requires new timekeeping software		
# Instruments	4	6-7	More 1553 remote terminals to manage		
RS-422?	No	Yes	New driver needed; high speed I/O changes system scheduling and timing		
Max science rate	55 kbps	450 kbps	Higher max. recording rate decreases flexibility in SSR management		
Max downlink	4 Mbps	800 kbps	Lower max. downlink rate increases flexibility in SSR management		
Broadcast?	No	Yes	New software needed to collect broadcast data, select between		





### **G&C S/W Requirements**

- Maintain spacecraft attitude safety
- Support spacecraft operational requirements
  - High gain antenna pointing
  - Solar panel alignment
  - Autonomous momentum management
- Support instrument requirements
  - Maintain solar pointing within long term and jitter specifications
  - Provide Sun keep-in violation, momentum dump warnings
- Generate G&C system telemetry
  - Attitude history
  - Anomalous event dumps
  - Routine G&C status and health reports





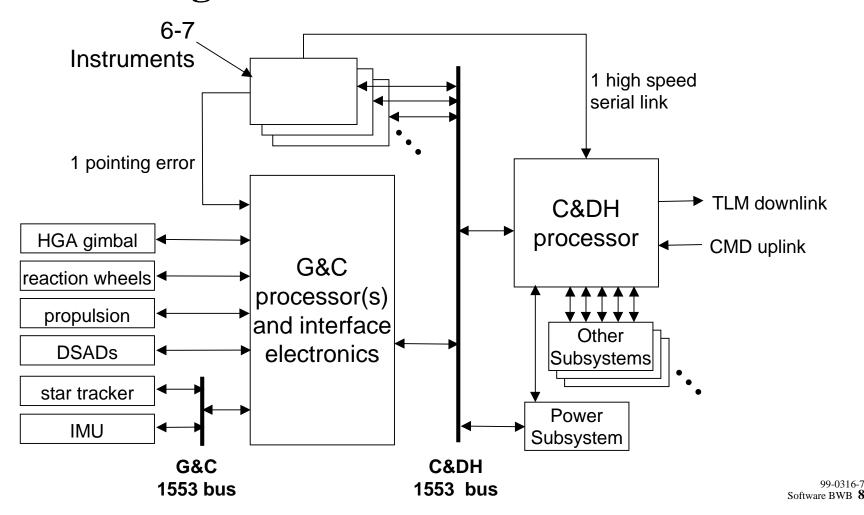
### **G&C** Requirements vs. TIMED

Feature	TIMED	STEREO	Software Impact			
H/W redundant?	Yes	No	Requires new S/W loading approach			
GPS?	Yes	No	Requires new orbit determination software			
Momentum management	Torque rods	Cold gas	Requires new I/O and control software			
Star tracker, IMU, etc.	Known	TBD	Requires new I/O and control software if devices differ from TIMED			
High gain antenna	No	Yes	Requires new I/O and control software for gimbal			
Error signal	No	Yes	Requires new I/O and control software			
Control update frequency	10 Hz	TBD	Unknown until further analysis; could help or hurt processor margins			





#### Flight Software Environment







#### **C&DH Software Baseline**

#### TIMED architecture

- Reuse requirements document as starting point
- 12 MHz Mongoose running Nucleus+ RTOS
- Same approach to uplink, downlink, 1553 bus management
- Add drivers for RS-422 high speed link
- Delete instrument daily packet quota enforcement
- Power management requirements TBD

#### Load estimates

- CPU usage: 25% (based on TIMED estimates updated for STEREO)
- Memory: TIMED is under 30% usage of code space (RAM and flash), assuming 50% of memory is available for code





#### **G&C Software Baseline**

- TIMED software architecture
  - 12 MHz Mongoose running Nucleus+ RTOS, with RTX2010 based Attitude Interface Electronics
  - Reuse requirements documents as starting point
  - Eliminate attitude processing in AIE to reduce complexity and regain processor and memory margin
  - Use RTW again to automatically generate attitude "c" code for GCC
- Load estimates
  - CPU usage: AIU usage about 25%; GCC unmeasured
  - Memory: TIMED AIU uses over 85% of RAM; GCC uses
     <30% of RAM allocated for code</li>





### **I&T S/W Requirements**

- Deliver commands to S/C and instruments at bench system
- Assess and archive spacecraft telemetry
- Deliver instrument telemetry to instrument teams
- Provide visibility into internal spacecraft interfaces for test purposes
- Support multiple hardware configurations as integration proceeds
- Support test scripting, data collection, and problem reporting and resolution





### **Mission Operations S/W Requirements**

- Deliver and log commands for two spacecraft and their instruments
- Receive and distribute all downlink telemetry
- Monitor spacecraft health and safety
- Assess and archive spacecraft telemetry data
- Produce and distribute time correlation and navigation data
- Maintain spacecraft command and telemetry dictionaries
- Support spacecraft activity planning
- Maintain configuration control of uploadable software and parameters





#### Mission Operations Requirements vs. TIMED

Feature	TIMED	STEREO	Software Impact		
# spacecraft	1	2	Requires separate command and telemetry databases, sorting commands and telemetry by spacecraft, and supporting 2 passes simultaneously		
Ground station	APL/ LEO-T	DSN	Requires changes to contact planning		
GPS?	Yes	No	Requires ground-based navigation team with interfaces to DSN		
Unsupported passes	Goal	Weekend	Requires up-front commitment to more automated operations		





#### **GSE Software**

#### G&C testbed

- Connects to G&C computer; accessible via Ethernet
- Simulates G&C system components and environment
- Allows real time closed loop tests of the attitude system
- Becomes part of the real time spacecraft simulator after launch

#### C&DH testbed

- Connects to C&DH computer; accessible via Ethernet
- Simulates C&DH interfaces and environment
- Allows real time tests of C&DH hardware and software





### **GSE Software (con't)**

- Mini-MOC (if implemented)
  - Is a stripped-down version of the MOC, available early in the program, for use in G&C and C&DH subsystem testing.
  - Can command and receive telemetry from both the subsystem under test and supporting GSE
  - Uses the same command and telemetry dictionaries, command procedures, and display pages as the MOC
- Spacecraft emulator (if implemented)
  - Accessible via Ethernet
  - Connects to instruments via their spacecraft interfaces (1553, serial)
  - Emulates spacecraft functions that support instruments
  - Allows instrument checkout before spacecraft integration
  - TIMED provided one emulator to each instrument developer

99-0316-7 Software BWB **16** 





#### Trade Studies for Phase A/B

- Elimination of the processor in the AIE
  - G&C computer would manage all attitude tasks
  - Trade study must ensure the G&C computer would not be overloaded
  - TIMED AIE boot and application software were costly
  - AIE's RTX 2010 development tools are no longer supported
- Selective SSR playback to allow direct replay of missed transfer frames without playing back a whole segment
- Use of variable length packets
  - Study whether benefits of variable length packets outweigh costs





#### Trade Studies for Phase A/B (con't)

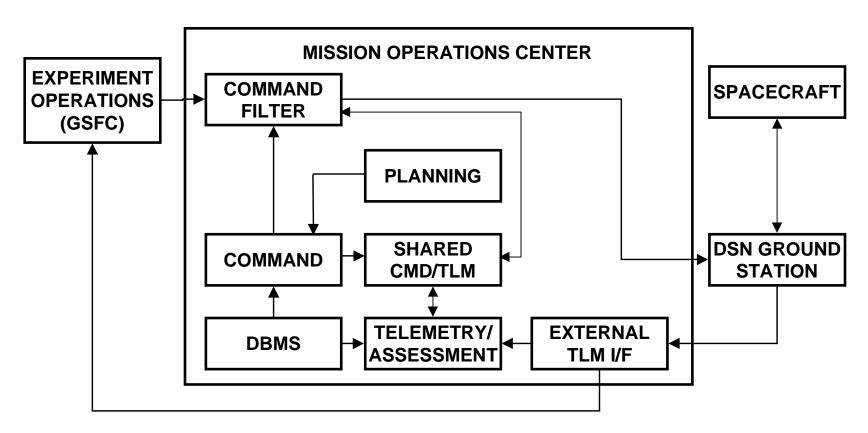
- Operating systems, tools
  - Nucleus+ (TIMED RTOS for Mongoose), VxWorks, VRTX
  - TASKING (TIMED development tools for Mongoose), gnu
- Use of EPOCH for Mission Operations Center
- Implementation of Mini-MOC, spacecraft emulator
  - Cost/benefit tradeoff





### **Mission Operations S/W Baseline**

(Based on TIMED EPOCH 2000 System)







### **Technology Insertion Candidates**

- Use of commercially available file system extensions to Real Time Operating System
  - Code and parameter upload and download operations become simple file transfers
  - Easy, familiar model for Mission Operations
- Non-coherent Doppler navigation (with JHU/APL-supplied hardware and software at DSN ground stations)
- Unattended weekend operations





### **RF** Communications

#### U. I. VonMehlem

The Johns Hopkins University Applied Physics Laboratory 11100 Johns Hopkins Road Laurel, MD 20723-6099





#### General

- Two-year mission life
- Five-year goal
- X-band TWT A, designed for two-year mission life plus <18 month ground operation.
- Primary DSN resource is existing 34m BWG antenna system, supplemented by 34 m HEF/upgraded 34m BWG and 70 m systems as required





#### General (con't)

- Simultaneous X-band uplink, X-band downlink and tracking
  - Uplink

• Normal mode: 125 bps

• Emergency: 7.8125 bps

- Downlink
  - Normal high rate science mode: >200 kpbs (when HGA pointing maintained within +0.1°)
  - Broadcast mode: 500 bps
  - Emergency mode: 10 bps





### **Uplink and Downlink**

- Margin is 3 dB (min); 6 dB goal on uplink
- BER ≤10E–6





#### **Downlink**

- High Rate Science
  - 5 Gbit downlink per DSN contact for two year mission life:
    - Translates to 200 kbps in 7-hr downlink time
    - At two years distance from Earth for baseline trajectory:
      - -Leading spacecraft (drift rate 20°/yr) is at 0.65 AU
      - -Lagging (drift rate 28°/yr) is at 0.97 AU
    - DSN resources are 34 m BWG antenna system supplemented with 34 m HEF and 70 m
    - Post launch/early operations 800 kbps max
  - Rate 1/6, k = 15 convolutional coding + RS
  - Bit rate spacing 3 dB (nominal)





### Downlink (con't)

- Broadcast mode:
  - 500 bps downlink rate:
  - -R = 1/2, k = 7 convolutional coding + RS
  - No uplink
  - X-band baseline:
    - Data downlinked through spacecraft HGA
    - TBS ground system, G/T is specified based on link
- S-band option:
  - Data downlinked through spacecraft dual feed X- and S-band HGA
  - NOAA ground system
- Emergency operation:
  - 34 m HEF and 70 m DSN resources





### **Navigation Support**

- Navigation support via two-way Doppler tracking using JHU/APL developed non-coherent tracking technique:
  - For the two year mission support:
    - 0.1 mm/s (over 60 sec measurement interval) Doppler accuracy
    - $\pm$  7500 km position accuracy
  - JHU/APL develop software. Where software resides (JHU/APL or JPL/DSN) will be negotiated with DSN during Phase A.
  - DSN provide to JHU/APL:
    - Product (raw Doppler information) from Radiometric Data Center
    - All spacecraft telemetry frames, frame number, frame synchronization time tags (a standard product)

99-0316-8 RF Comm VonMehlem **7** 





#### **RF** Communications

Additional Information - Preliminary Downlink Bit Rate Performance

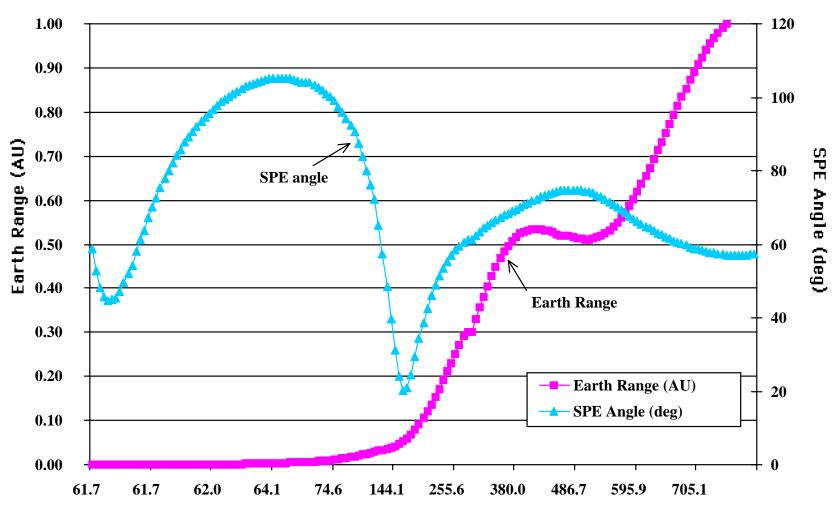
Judi von Mehlem





STEREO 28 deg/year Lagging Spacecraft

Earth Range and Sun-Probe-Earth Angle vs Elapsed Time since Leading S/C Launch

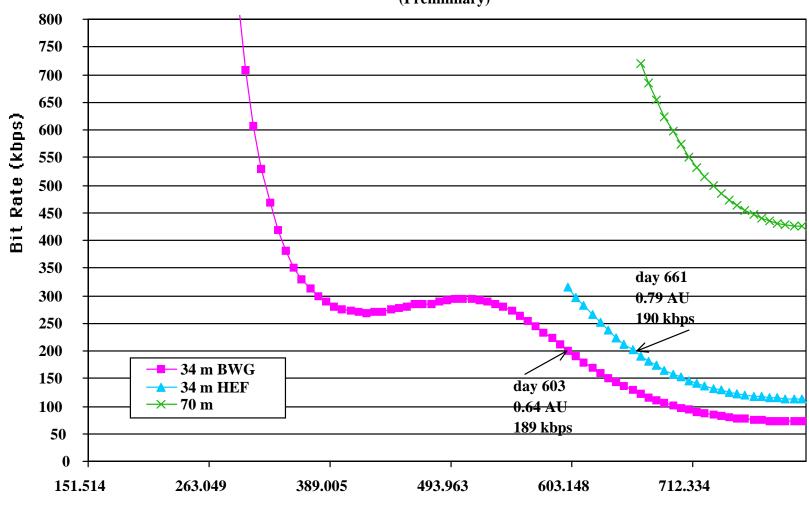


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STEREO 28 deg/year Lagging S/C
Bit Rate Capability S/C HGA to DSN Resources
(Preliminary)



EFaqued Time (daysinine dingreph cofrie ading spacecraft)





Bit rat pe formance deficienc ysumm ar for 2ds gy rlag gog spacer atf (Baeline is 40 WWTA; Im HGA; 3 dB link manig)

DSN a ntenna	S/C	T WTA	D a ¹y	E ath	Bit Ra t e	Link
s yste m	HGA	(w)		R ang e	(kbps)	M a ring
	( <b>m</b> )			(A U)		(dB)
Last ~ 1 daly s						
34m BW G	1.1	40	603	0.64	189 <sup>2</sup>	3
	1.1	40	603	0.64	200	2.7 <sup>2</sup>
	1.1	40	668	0.81	115	3
	1.1	40	734	0.97	82	3
			(2			
			y e ær			
	1.75	40	734	0.97	200	3
34m HEF	1.1	40	661	0.79	190 <sup>2</sup>	3
	1.1	40	734	0.97	128	3
	1.1	40	734	0.97	200	1
	1.4	40	734	0.97	200	3
	1.1	60	734	0.97	200	2.8 <sup>2</sup>
70 m	1.1	40	734	0.97	485	3

T able no tse

- 1. Relative to launch for the ading space crift (6 Oday is a life rthan la gingg space crift)
- 2. Bit rat eloce to 2 (kd ps or marign dose to 3 dB, within c acula ion a sumptions for pr ephase A





# • 28 DEG/YEAR LAGGIN SPACECRAFT TABLE ASSUMPTIONS:

- SPE angle is <105 deg throughout mission. SPE is only >90 within first 25 days of launch of lagging spacecraft. HGA is used for downlink when SPE<90 deg. Extended HGA (with 2 dB degradation) is used for SPE between 90 and 105 deg.
- Existing 34 m BWG performance is used

#### • CONCLUSION:

Link does not support 200 kbps using existing 34 m BWG from ~day 603 to ~day 734 (~131 days).





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# • 28 DEG/YEAR LAGGIN SPACECRAFT TABLE CONT:

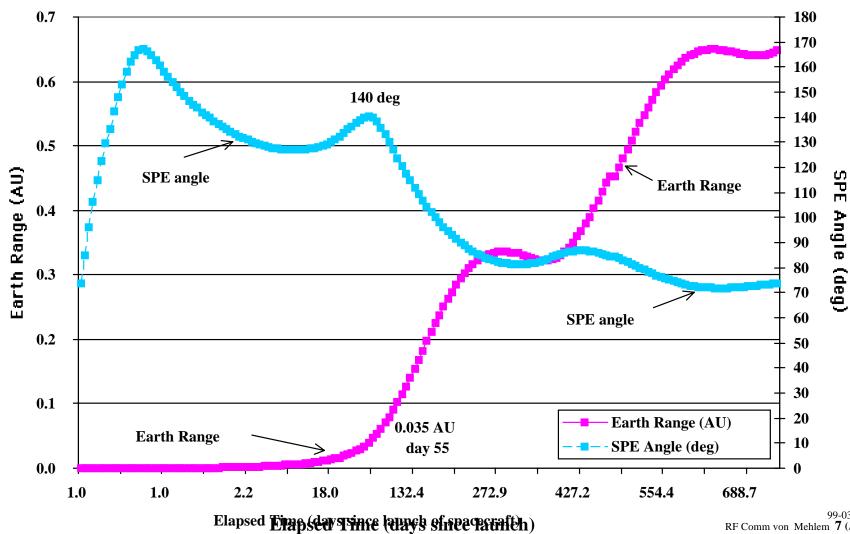
#### • MITIGATION:

- Increase HGA size (mechanical limitations with present launch vehicle)
- From ~day 603 to ~661 (~58 days) use 34m HEF (if 34m BWG is upgraded, could use it since performance is expected to approach HEF performance). From ~day 661 to ~734 (~73 days) use 70 m DSN system. (cost)
- Increase transmitter power (cost, dc power).
- Accept lower link margin (risk).





STEREO 20 deg/year Rate Leading Spacecraft Sun Probe Earth Angle and Earth Range vs Elapsed Time since S/C Launch



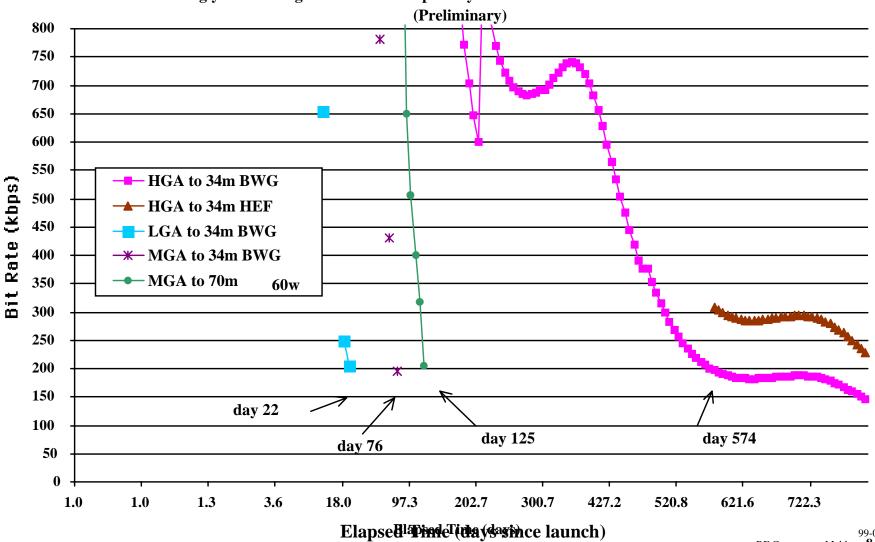
99-0316-8

RF Comm von Mehlem 7 (Add)





STEREO 20 deg/year Leading S/C- Bit Rate Capability S/C HGA to DSN Resources



99-0316-8 RF Comm von Mehlem **8 (Add)** 





Bit rat pe fo mance deficienc ysumm a rfor 2d0 gy rle aling spacer atf (Baeline is 40 WVTA; Im HGA; 3 dB link maring)

DSN a rtenna	S/C	T WTA	D a ¹y	E arth	Bit Ra t e	
s yste m	antenna	(w)		R ang e	(kbps)	M a ning
				(A U)		(dB)
Last ~ 2 datys						
34m BW G	1.1 m	40	574	0.63	196 <sup>2</sup>	3 <sup>2</sup>
	HGA					
	1.1 m	40	800	0.72	149	3 <sup>2</sup>
	HGA		(2			
			y e as)r			
	1.1 m	40	800	0.72	200	1.75
	HGA					
	1.1 m	60	800	0.72	223	3
	HGA					
	1.3 m	40	800	0.72	200	3.1
	HGA					
34m HEF	1.1 m	40	800	0.72	234	3
	HGA					
D a y-76 to						
$\sim 125^3$						
34m BW G	MGA	40	76	0.06	196 <sup>2</sup>	3
	MGA	40	90	0.08	73	3
	MGA	40	125	0.14	14	3
70 m	MGA	40	111	0.11	336	3
	MGA	40	125	0.14	88	3
	MGA	40	118	0.13	200	1
	MGA	60	118	0.13	200	3

#### T able no tse

- 1. L aunched 6 da y s a life rthan l a gingg spa c era f. 8 0 day mission life env do pes 2 y e a for rmission life f o raggin gspa ec r ft.
- 2. Within c acula ton assumptions fo rpr epha s A.
- 3. SPE is betwere 1 1 5 nd 1 4.3) de g(~2 de g).





# • 20 DEG/YEAR LAGGIN SPACECRAFT TABLE ASSUMPTIONS:

- LGA (based on NEAR) is used post launch until ~day 20. MGA (based on NEAR fanbeam) is used ~day 20 to 125. HGA used from ~day 125 through end of mission. SPE is >90 from day 125 to 209.
- Assume spacecraft is oriented about x-axis to maximize antenna gain towards earth.
- Existing 34 m BWG performance is used

#### • CONCLUSION #1:

Link does not support 200 kbps using existing 34 m BWG from ~day
 574 to ~day 800 (~226 days).





# • 20 DEG/YEAR LAGGIN SPACECRAFT TABLE CONT:

#### • MITIGATION:

- Use 34m HEF (if 34m BWG is upgraded, could use it since performance is expected to approach HEF performance).
- Increase transmitter power (cost, dc power).
- Increase HGA size (mechanical limitations with present launch vehicle)

#### CONCLUSION #2:

Link does not support 200 kbps using existing 34 m BWG from ~day
 76 to ~day 125 (~49 days).





#### • MITIGATION:

- Redesign NEAR fanbeam antenna to provide more gain over smaller beamwidth (mechanical limitations with launch vehicle and spacecraft hardware, cost) or design a new antenna (cost).
- Use 70 m DSN system and higher power (cost, dc power).
- Use 70 m DSN system and accept lower link margin (cost, risk).
- Slew spacecraft to direct HGA at earth (loose science during downlink)
- Redesign trajectory to move second peak of high SPE earlier in mission (may not be possible, science impact).
- Have second small (~9 in) gimballed dish (mechanical constraints on spacecraft, costly.





#### **Orbit Determination**

Gene A. Heyler

The Johns Hopkins University Applied Physics Laboratory 11100 Johns Hopkins Road Laurel, MD 20723-6099



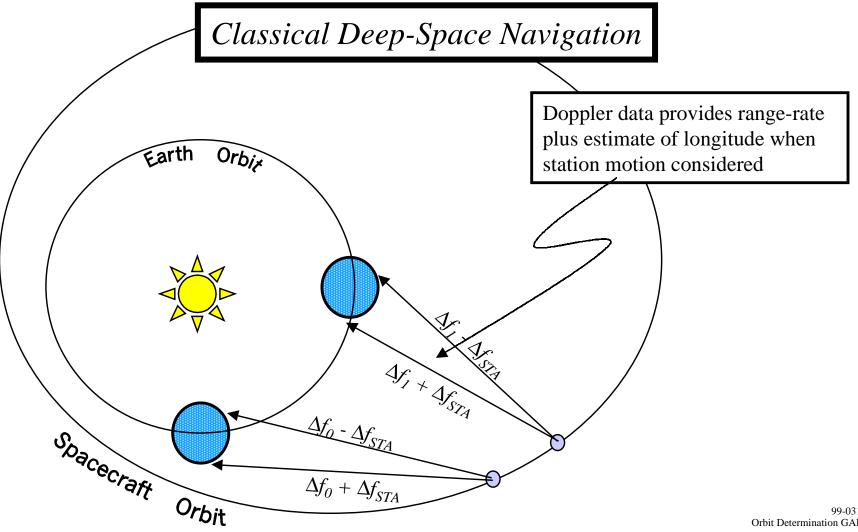


#### **Navigation Characteristics**

- Singular Doppler data provides range-rate (0-D solution)
- Station motion over one day provides 1-D solution (longitude)
- Add ranging to produce 2-D solution
- Add N/S stations or solar angles to get 3-D solutions
- Need change in Doppler data over time
  - STEREO in nearly identical Earth orbit
  - Fitting arcs very long (weeks or months)
  - Hi-fidelity radiation pressure model needed
    - Need dynamic cross-sectional area model
    - Need attitude information

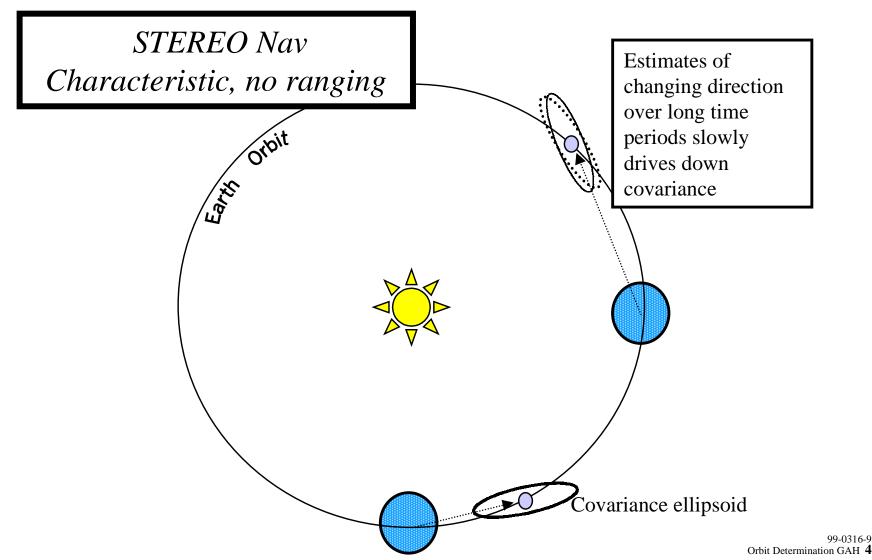






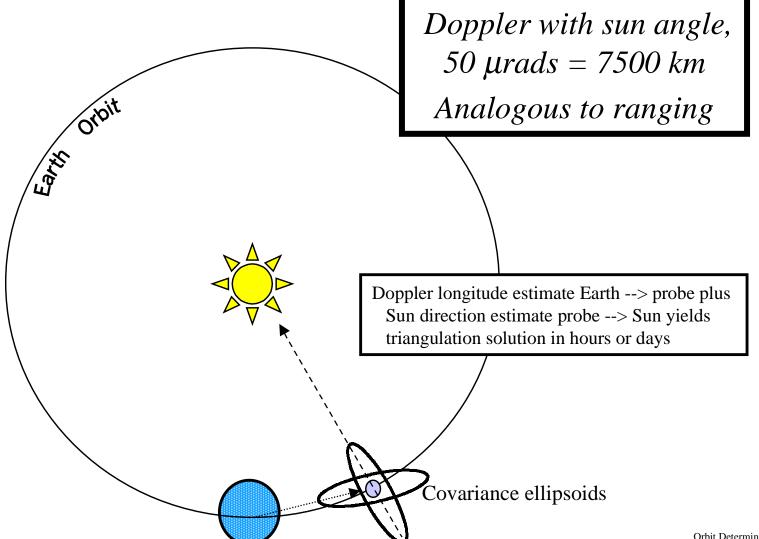
















#### **Spacecraft Sun Angle Experimental Data**

- Triangulation method determines Earth -> probe range
- Convergence time drops from weeks/months to hours/day
- Minimizes need for hi-fidelity radiation pressure model
- Possibly good to 50 µrads, would meet 7500 km requirement
- Inclusion in ground processing filter
- Needed for any onboard autonomous nav experiments





#### **Navigation Ground Software**

- Acquire/[modify] existing systems
- Have narrowed candidates down to:

GTDS-Goddard Trajectory Determination System OCEAN-Orbit Covariance Estimation and Analysis

- Currently determining capabilities of each
- TBD–ease of modifiability





#### GTDS-Goddard Trajectory Determination System

- Old reliable, currently used on ~40 missions
- Vintage 1970's, batch, mainframe, Fortran, card punch format
- Installed and tested on JHU/APL Unix machines
- Source code, makefiles transmitted to JHU/APL, no known license problems
- Documentation delivered
- Ephemeris generator, orbit determination, test generation modules
- Hi-fidelity solar system and atmospheric models
- Determine modifiability





#### OCEAN-Orbit/Covariance Estimation and Analysis

- Developed by Naval Research Lab (circa 1995, ongoing)
- Backup support for 12 operational LEO satellites (automated)
- Executable and documentation (no source) provided to support TIMED Guidance and Navigation System (GNS) validation
- Supported on DEC (VMS, Ultrix) and SGI (IRIX)
- Batch or filter based estimation (method is observation type dependent)
- Hi-fidelity solar system and atmospheric models
- Determine modifiability





#### **Conclusions**

- Assume 'one-way non-coherent' Doppler
- Require Doppler data (range-rate) product
- Require RF ranging product (especially early in mission)
- Require solar angle (SCIP centroiding data) plus S/C attitude for alignment calculations and navigation option
- Require orbit determination software support
  - Baselining GTDS or OCEAN
  - Steep learning curve
  - Installation, testing, enhancements
  - Interface software development